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# Effect of lanthanide promotion on catalytic performance of sol-gel Ni/Al<sub>2</sub>O<sub>3</sub> catalysts in steam reforming of propane

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#### Abstract

The effect of lanthanide elements (La, Ce, and Yb) on the catalytic behavior of sol–gel Ni/Al<sub>2</sub>O<sub>3</sub> catalysts in propane steam reforming was investigated. Steady-state reaction experiments show that the addition of small amounts (2 wt.%) of lanthanide elements improves the catalytic activity and stability significantly. The changes in reaction performance are related to catalyst reducibility, nickel surface area and resistance to deactivation. Temperature-programmed reduction (TPR) and X-ray photoelectron spectroscopy (XPS) characterization results reveal that the presence of lanthanide elements enhances the catalyst reducibility; the positive effect is most evident with 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts. H<sub>2</sub> chemisorption data indicate that 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts exhibit larger nickel surface area compared to 20% Ni/Al<sub>2</sub>O<sub>3</sub> catalysts. Nickel surface area of sol–gel catalysts is also found to be strongly dependent on calcination and reduction temperatures. In situ DRIFTS experiments coupled with TPD and TPReaction suggest that formate and carbonate species are formed upon the reaction of adsorbed propane and water on reduced catalysts.

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#### 1. Introduction

Hydrogen is the ultimate clean energy carrier. When it is combusted, heat and water are the only products. When it is used as a fuel for fuel cells, then it has the potential of providing much higher efficiencies compared to combustion. Thus, hydrogen offers a potentially non-polluting and efficient fuel for today's rising energy demands [1]. However, in the transition period before renewable sources of hydrogen can be developed, production of hydrogen from fossil fuels remains an important technology. Currently, steam reforming of natural gas, which is composed mainly of methane, is used to produce most of hydrogen in US and about half of the world's hydrogen supply. Naphtha fractions with a final boiling point of less than 220 °C are also considered as suitable feedstocks for hydrogen production [2]. However, current Ni-based catalysts, which are used for natural gas steam reforming processes, suffer from catalyst deactivation by coke formation more severely when higher hydrocarbons are reformed at low steam/carbon ratios.

Although supported precious metals such as Pd, Pt, and Rh have been reported to be active and stable for steam reforming of hydrocarbons [3–8], the cost of the precious metals is still a major drawback. The low-cost and long-proven performance of Ni-based catalysts, therefore, warrant the effort to optimize these catalysts for steam reforming applications, particularly fuel processing technology from existing liquid fuels such as gasoline and diesel.

There is evidence in the literature pointing to an improvement in catalytic activity of Ni-based catalysts in hydrocarbon steam reforming with the addition of lanthanide elements [9–11]. Zhuang et al. [9] investigated the effect of cerium oxide as a promoter in supported Ni catalysts for methane steam reforming. It showed a beneficial effect by not only decreasing the carbon deposition rate, but also increasing the steam reforming activity. The authors believed that cerium oxide accelerated the reaction of steam with

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adsorbed species on the nickel surface, thus decreasing the carbon deposition as well as increasing or maintaining the catalytic activity. Su and Guo [10] also reported an improvement in catalytic activity and resistance to Ni sintering of Ni/Al<sub>2</sub>O<sub>3</sub> catalysts doped with rare earth oxides in methane steam reforming. The growth of Ni particles and the formation of inactive NiO and NiAl<sub>2</sub>O<sub>4</sub> phases were suppressed by the addition of rare earth oxides. Moreover, the oxides of heavy rare earth elements (Gd, Er, Dy) exhibited a more pronounced effect than those of the light ones (La, Pr, Nd).

The use of lanthanide-promoted Ni/Al2O3 catalysts in dry reforming of methane [12–15] and benzene hydrogenation [16] has also been reported. The effects of the addition of lanthanide oxides (La<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub>) and preparation procedures were investigated in the reforming of methane with carbon dioxide over impregnated Ni/Al<sub>2</sub>O<sub>3</sub> catalysts [12]. When lanthanides were impregnated prior to nickel, an enhanced reducibility of nickel and a decrease in nickel particle size were observed. However, the reforming activity was not affected to a large extent by the impregnation order of nickel and lanthanides. The presence of CeO<sub>2</sub> (1-5 wt.%) in impregnated Ni/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalysts was found to reduce the chemical interaction between nickel and the alumina support, resulting in an increase in reducibility and higher nickel dispersion [13,14]. Moreover, carbon deposition was greatly suppressed due to the oxygen storage capacity of CeO<sub>2</sub>. The catalytic activity, sulfur tolerance, and thermal stability were remarkably improved after adding La, Sm, and Yb into Ni-B/Al<sub>2</sub>O<sub>3</sub> catalysts for benzene hydrogenation [16]. The positive effect of lanthanide promotion was associated with easier reduction of nickel oxides, smaller nickel particles, and larger surface area of active nickel.

In this study, Ni/Al<sub>2</sub>O<sub>3</sub> catalysts promoted with lanthanide elements (La, Ce, and Yb) were prepared by a modified sol–gel technique and were examined in propane steam reforming. Characterization was performed using the BET N<sub>2</sub> adsorption method, X-ray diffraction (XRD), temperature-programmed reduction (TPR), X-ray photoelectron spectroscopy (XPS), and H<sub>2</sub> chemisorption. In situ DRIFTS studies were also conducted to identify adsorbed species under  $C_3H_8$  and  $C_3H_8 + H_2O$  flows as well as to elucidate the reaction pathways for propane steam reforming.

#### 2. Experimental

#### 2.1. Catalyst preparation

Catalysts were prepared using a modified sol-gel technique. Nickel and lanthanide precursors (Aldrich) used were in nitrate form. For the aluminum precursor, aluminum tri*sec*-butoxide (ATB; Aldrich) was used. Ethanol (Alfa Aesar; 130 cm<sup>3</sup>) was used as the solvent. The following sol-gel parameters were varied during the synthesis: nickel content = 10-25 wt.%, lanthanide content = 2-5 wt.%, H<sub>2</sub>O/ATB molar ratio = 3.6-5.0, and pH of the resulting gels = 4.8-8.5. Initially, ATB was placed in ethanol and stirred. The aqueous solutions with the desired amounts of nickel and lanthanide were added dropwise into the suspension using a syringe pump at the flow rate of  $0.5 \text{ cm}^3/\text{min}$ . It is noted that the aqueous lanthanide nitrate solution was added first followed by that of nickel. The pH of the resulting green gel was measured and adjusted by adding HNO<sub>3</sub> (Fisher) or NH<sub>4</sub>OH (Fisher). The gels were stirred for an additional 15 min and were kept at room temperature for 30 min. The samples were then dried overnight in the oven at 110 °C to remove the remaining water and ethanol. The dry samples were ground to a fine powder and were calcined under  $O_2$  at 450 °C (ramp rate = 10 °C/min) for 4 h.

#### 2.2. Catalyst characterization

BET surface areas of calcined catalysts were measured by N<sub>2</sub> adsorption-desorption at 77 K using a Micromeritics ASAP 2010 instrument. Before measurements, samples were degassed under vacuum at 130 °C overnight. XRD patterns of calcined and reduced catalysts were obtained with a Bruker D8 Advance X-ray diffractometer equipped with atmosphere and temperature control stage and using Cu Ka radiation ( $\lambda = 1.542$  Å) operated at 40 kV and 50 mA. In this experiment, 5% H<sub>2</sub>/N<sub>2</sub> was used as a reducing agent. TPR of catalysts was conducted using a laboratory-made gas flow system described in detail elsewhere [17]. Catalyst samples (50 mg) were placed in a 1/4 in. o.d. quartz U-tube reactor. The catalysts were then re-calcined under 10% O<sub>2</sub>/He at 450 °C for 1 h followed by cooling to room temperature under Ar. The reduction was performed with 10% H<sub>2</sub>/Ar  $(40 \text{ cm}^3 \text{ (STP)/min})$ . The temperature of the catalysts was raised using a ramp rate of 10 °C/min to 900 °C and held at that level for 10 min. The effluent from the reactor was passed through a silica gel water trap to remove moisture formed during reduction. H<sub>2</sub> consumption was measured using a thermal conductivity detector (TCD) connected to a data-acquisition computer.

XPS of reduced catalysts was performed with an AXIS Ultra XPS spectrometer with an Al anode operated at 14 kV and 10 mA. Reduction was performed with 20% H<sub>2</sub>/N<sub>2</sub> at 600 °C for 2 h. Prior to the measurements, all reduced catalysts were kept in tightly sealed reactors and were subsequently mounted on a sample holder with conductive tape in a dry glovebox filled with Ar. The sample holder was then carefully transferred to the analysis chamber of the spectrometer with a controlled-atmosphere transporter. Spectra were corrected using the C 1s signal located at 284.5 eV.

 $H_2$  chemisorption of catalysts was conducted using a Micromeritics ASAP 2010 Chemisorption System. Prior to adsorption measurements, calcined samples (0.2 g) were reduced under  $H_2$  at the desired reduction temperature for 2 h. Subsequently, the samples were cooled down to 35 °C

followed by evacuation to  $10^{-5}$  mmHg. The adsorption isotherms were measured at equilibrium pressures between 50 and 500 mmHg. H<sub>2</sub> uptakes at monolayer coverage of the Ni crystallites were used to estimate Ni dispersion and metallic surface area, assuming that each surface Ni atom chemisorbs one hydrogen atom (H/Ni<sub>surface</sub> = 1).

DRIFTS experiments were performed using a Bruker IFS66 instrument equipped with an MCT detector and a KBr beamsplitter. Catalysts were reduced under 20% H<sub>2</sub>/N<sub>2</sub> at 600 °C for 2 h and then were placed in a sample cup inside a Spectratech diffuse reflectance cell equipped with KBr windows and a thermocouple that allowed direct measurements of the surface temperature. Spectra for each experiment were averaged over 1000 scans in the mid-IR range  $(400-4000 \text{ cm}^{-1})$  to a nominal  $3 \text{ cm}^{-1}$  resolution. Prior to the collection of spectra, the catalysts were re-reduced in situ under 20% H<sub>2</sub>/He at 450 °C for 1 h. The background spectra were taken at different temperature intervals under He. The adsorption of C<sub>3</sub>H<sub>8</sub> was performed at room temperature for 1 h followed by flushing under He for 30 min. The spectra were subsequently collected at different temperatures up to 450°C.

#### 2.3. Reaction studies

The steady-state reaction experiments were performed using a stainless steel fixed-bed flow reactor (1/4 in. o.d.). Catalysts were compared in propane steam reforming using equal surface area loading  $(9 \text{ m}^2)$  in the reactor at 400–550 °C and  $H_2O/C = 1.3$ . The feed percentages for these experiments were  $C_3H_8/H_2O/N_2 = 1/4/95$  (feed flow rate = 300–400 cm<sup>3</sup> (STP)/min). Unless otherwise noted, catalysts were reduced in situ under 20%  $H_2/N_2$  (50 cm<sup>3</sup> (STP)/min) at 600 °C for 2 h prior to the reaction. The effluent from the reactor was analyzed using an automated Shimadzu GC-14A equipped with FID and TCD detectors. Separations were performed under Ar using two columns: Porapak Q ( $12 \text{ ft} \times 1/8 \text{ in. SS}$ , 80/100 mesh) and Molecular Sieve 13X (5 ft  $\times$  1/8 in. SS, 60/80 mesh). A GOW-MAC 069-50 ruthenium methanizer operated at 350 °C was used with the FID for the sensitive determination of CO as low as 10 ppm. Reaction data were taken after steady state was reached. Conversion, yield, and selectivities were defined as follows:

$$%C_{3}H_{8} \text{ conversion} = \left(\frac{\text{moles of carbon converted}}{\text{total moles of carbon in the feed}}\right) \times 100$$

$$\% H_2 \text{ yield} = \left(\frac{2 \times \text{moles of } H_2 \text{ produced}}{\text{total moles of hydrogen in the feed}}\right) \times 100$$

%C-product selectivity for A

$$= \left(\frac{\text{moles of C in product A}}{\text{moles of C in all carbon - containing products}}\right) \times 100$$

%H-product selectivity for B

$$= \left(\frac{\text{moles of H in product B}}{\text{moles of H in all H} - \text{containing products}}\right) \times 100$$

C-containing products are CO, CO<sub>2</sub>, and CH<sub>4</sub>. Hcontaining products are H<sub>2</sub> and CH<sub>4</sub>. Reproducibility of the results were tested using different catalyst batches run under identical conditions.

#### 3. Results and discussion

#### 3.1. Physical properties of sol-gel catalysts

The effect of synthesis parameters on the physical properties of sol-gel Ni/Al<sub>2</sub>O<sub>3</sub> catalysts is reported in Table 1. Parameters that were varied during the synthesis included Ni content, pH of the resulting gels, and H<sub>2</sub>O/ATB molar ratio. BET surface area of sol-gel Ni/Al<sub>2</sub>O<sub>3</sub> catalysts is seen to decrease with increasing Ni contents possibly due to nickel aggregation to form larger particles on the Al<sub>2</sub>O<sub>3</sub> support surface during thermal treatment. The decrease in surface area is even more pronounced at higher Ni contents. Furthermore, an increase in pH and H2O/ATB ratio causes an increase in surface area of 20 wt.% Ni/Al<sub>2</sub>O<sub>3</sub> catalysts. It is noted that a decrease in the pore diameter from 10.5 to 7.4 nm occurs when  $H_2O/ATB$  ratio is increased from 3.6 to 5.0. This phenomenon is related to an increase in cross-linking as a result of an increase in the extent of hydrolysis at high H<sub>2</sub>O/ATB ratios [18].

BET surface areas of lanthanide-promoted sol-gel Ni/Al<sub>2</sub>O<sub>3</sub> catalysts prepared at different lanthanide contents are listed in Table 2. In general, catalysts have a lower surface area than the pure support. At lower loading levels, the lanthanide-promoted catalysts exhibit a higher surface area than the unpromoted catalyst, but a loss in surface area with higher lanthanide content is observed with Ni–Ce/Al<sub>2</sub>O<sub>3</sub> and Ni–Yb/Al<sub>2</sub>O<sub>3</sub> catalysts possibly due to pore blockage by excess metal. In addition, an increase in calcination temperature from 450 to  $600^{\circ}$ C causes a decrease in surface area

Table 1 BET surface area of various sol-gel Ni/Al<sub>2</sub>O<sub>3</sub> catalysts

Synthesis parameter	Surface area (m <sup>2</sup> /g)		
Ni content (wt%)	pН	H <sub>2</sub> O/ATB ratio	
10	4.8	3.6	248
15	4.8	3.6	244
20	4.8	3.6	209
25	4.8	3.6	180
20	4.8	3.6	209
20	7.0	3.6	215
20	8.8	3.6	259
20	4.8	3.6	209
20	4.8	4.0	203
20	4.8	5.0	248

Table 2

BET	surface	area	of	lanthanide	-promoted	sol-gel	Ni/Al <sub>2</sub> O <sub>3</sub>	catalysts	cal-
cined	l at 450 °	°C							

Catalyst	Surface area (m <sup>2</sup> /g)
20% Ni/Al <sub>2</sub> O <sub>3</sub>	209
20% Ni-2% La/Al <sub>2</sub> O <sub>3</sub>	286
20% Ni-5% La/Al <sub>2</sub> O <sub>3</sub>	300
20% Ni-2% Ce/Al <sub>2</sub> O <sub>3</sub>	304
20% Ni-5% Ce/Al <sub>2</sub> O <sub>3</sub>	228
20% Ni-2% Yb/Al <sub>2</sub> O <sub>3</sub>	278
20% Ni-5% Yb/Al <sub>2</sub> O <sub>3</sub>	234
Al <sub>2</sub> O <sub>3</sub>	342

of Ni–Ce/Al<sub>2</sub>O<sub>3</sub> catalysts. The surface area of the catalyst calcined at 600  $^{\circ}$ C is 261 m<sup>2</sup>/g compared to 304 m<sup>2</sup>/g for the catalyst calcined at 450  $^{\circ}$ C.

#### 3.2. X-ray diffraction

The XRD patterns of calcined and reduced 20% Ni-2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts are compared in Fig. 1. The support calcined at 450 °C is relatively amorphous as evidenced by broad peaks that correspond to  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> (Fig. 1a). The possible crystalline phases in the catalyst calcined at 450 °C are NiO, NiAl<sub>2</sub>O<sub>4</sub>, and γ-Al<sub>2</sub>O<sub>3</sub> (Fig. 1b). However, XRD results are not conclusive about the presence of any Ni-containing crystalline phases, suggesting a high-level of dispersion of Ni. Furthermore, no cerium-related crystalline phases are detected, suggesting that cerium species could be well dispersed over the alumina support or could exist within the NiO matrix undetectable by XRD. After in situ reduction under 5%  $H_2/N_2$  at 600 °C, significant amounts of metallic nickel were formed as confirmed by the diffraction lines of a metallic nickel phase [(111), (200), (220)] at  $2\theta = 44.5^{\circ}$ ,  $51.8^{\circ}$ , and 76.4 $^{\circ}$ , respectively (Fig. 1c).



Fig. 1. XRD patterns of (a) sol–gel Al<sub>2</sub>O<sub>3</sub> calcined at 450  $^{\circ}$ C (b) 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst calcined at 450  $^{\circ}$ C (c) 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst reduced at 600  $^{\circ}$ C.



Fig. 2. TPR profiles of various sol-gel 20% Ni/Al<sub>2</sub>O<sub>3</sub> catalysts promoted with 2 wt.% lanthanide elements (calcined at 450 °C). The effect of calcination temperature on reducibility of 20% Ni-2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts is shown as an inset.

# 3.3. Promotion effect on catalyst reducibility and nickel surface area

#### 3.3.1. Temperature-programmed reduction

TPR experiments on lanthanide-promoted sol-gel Ni/Al<sub>2</sub>O<sub>3</sub> catalysts were performed using 10% H<sub>2</sub>/Ar as a reducing agent. As shown in Fig. 2, the TPR profiles exhibit two peaks, representing two different reduction sites on all catalysts. A small low-temperature (LT) reduction peak around 400 °C could be assigned to the reduction of trace amounts of NiO clusters. A broad high-temperature (HT) reduction peak above 500 °C could be due to the reduction of a well-dispersed and possibly amorphous NiO phase that interacts strongly with the alumina support. For lanthanide-promoted catalysts calcined at 450 °C, the position of the HT peak maximum shifts toward lower temperatures compared to that of the unpromoted catalyst. This suggests that the presence of lanthanide elements results in a greater reduction of nickel species; the promotion effect is most evident on the Ni-Ce/Al<sub>2</sub>O<sub>3</sub> catalyst. This could be due to a decreased interaction of Ni with the alumina support when a lanthanide element is present as a promoter. It is noted that the introduction of lanthanides to nickel catalysts showed no additional reduction peak under these conditions.

In general, calcination temperature plays a major role on the strength of metal oxide and support interaction for supported metal catalysts, which in turn strongly affects the degree of reduction. The effect of calcination temperature on the catalyst reducibility of Ni–Ce/Al<sub>2</sub>O<sub>3</sub> was also investigated. An increase in calcination temperature from 450 to 600 °C results in a shift of the HT peak maximum to a higher temperature around 680 °C as displayed in an inset (Fig. 2). Moreover, the reduction peak at 400 °C is more prominent with the catalyst calcined at 600 °C implying that the formation of crystalline NiO could be enhanced as the calcination temperature is increased. TPR results show that the interaction of Ni species with the alumina support becomes stronger at higher calcination temperatures, thus suppressing the reduction of Ni species to metallic Ni [19,20]. This could also be indicative of the formation of a nickel aluminate spinel at higher calcination temperatures.

#### 3.3.2. X-ray photoelectron spectroscopy

XPS was further conducted to study the nature of surface nickel species over the catalysts after reduction under 20%  $H_2/N_2$  at 600 °C for 2 h. The catalysts were transferred to the XPS chamber without exposing them to the atmosphere. The Ni 2p spectra of reduced lanthanide-promoted catalysts are shown in Fig. 3. The Ni 2p spectra of the catalysts exhibit features that are assigned to Ni<sup>2+</sup> with Ni 2p<sub>3/2</sub> and Ni 2p<sub>1/2</sub> binding energies at 855.8 and 873.3 eV, respectively and Ni<sup>0</sup> with Ni 2p<sub>3/2</sub> and Ni 2p<sub>1/2</sub> binding energies at 852.7 and



Fig. 3. Ni 2p X-ray photoelectron spectra of lanthanide-promoted sol–gel 20% Ni/Al\_2O\_3 catalysts reduced at 600  $^\circ\text{C}.$ 

Table 3

Comparison of the  $A_{\rm Ni}{}^0/(A_{\rm Ni}{}^0 + A_{\rm Ni}{}^{2+})$  XPS ratio of the catalysts after reduction at 600 °C

Catalyst	$A_{\rm Ni}{}^0/(A_{\rm Ni}{}^0 + A_{\rm Ni}{}^{2+})$
20% Ni/Al <sub>2</sub> O <sub>3</sub>	0.51
20% Ni–2% La/Al <sub>2</sub> O <sub>3</sub>	0.51
20% Ni-2% Ce/Al <sub>2</sub> O <sub>3</sub>	0.55
20% Ni-2% Yb/Al <sub>2</sub> O <sub>3</sub>	0.54

870.2 eV, respectively [21–24]. The Ni  $2p_{3/2}$  signal corresponding to Ni<sup>2+</sup> is accompanied by a broader peak located at 860.8 eV due to a strong shake-up process [25]. Ni 2p spectra indicate that the reduction of nickel species to the metallic state in the sol–gel catalysts is not complete due to a strong interaction of nickel oxide with the alumina support. It is noted that the satellite peak at 860.8 eV still remains in XPS spectra following TPR experiments (not shown). This suggests that the signal of Ni<sup>2+</sup> species could be due to NiAl<sub>2</sub>O<sub>4</sub>, which is more difficult to reduce. However, the possibility of a NiO phase cannot be excluded since the Ni 2p binding energies for these two species are very close together. In addition, all catalysts show similar Ni 2p spectra, suggesting that nickel species in these catalysts exist in a similar coordination environment.

Deconvolution of the Ni 2p spectra was performed by Gaussian–Lorentzian curve-fitting method to determine the peak areas for obtaining relative surface concentrations of nickel species. The ratio of peak areas  $A_{Ni}^{0}/(A_{Ni}^{0} + A_{Ni}^{2+})$  is used to illustrate the degree of reducibility. As displayed in Table 3, an increase in the  $A_{Ni}^{0}/(A_{Ni}^{0} + A_{Ni}^{2+})$  ratio for lanthanide-promoted Ni/Al<sub>2</sub>O<sub>3</sub> catalysts is seen after reduction compared to that of the unpromoted catalyst, indicative of an enhancement in the catalyst reducibility with lanthanide promotion. This is in agreement with TPR results obtained with the lanthanide-promoted catalysts, which have shown a shift in the maximum of the high-temperature peak corresponding to the reduction of NiO toward lower temperatures.

#### 3.3.3. $H_2$ chemisorption

 $H_2$  chemisorption was performed to determine nickel dispersion and nickel surface area of the catalysts. Unless otherwise noted, the reduction was conducted under  $H_2$  (UHP, 99.999%) at 600 °C for 2 h. The catalysts were then evacuated at 610 °C to remove adsorbed hydrogen from the surface and cooled to 35 °C. The first analysis was performed to measure both strong and weak sorption in combination whereas a repeat analysis was conducted to measure only weak (reversible) hydrogen uptake. The difference in the volume of hydrogen adsorbed from the first and repeat analyses was then plotted versus the hydrogen pressure and was extrapolated to zero pressure to obtain hydrogen uptake due to chemisorption on nickel. The nickel dispersion and nickel surface area were calculated assuming that one hydrogen atom is adsorbed on one surface nickel atom [26–28].

As listed in Table 4, the nickel dispersion is observed to be quite poor (2.3-6.4%) for all catalysts. The apparent low

Table 4  $$\rm H_2$$  chemisorption data on various lanthanide-promoted sol-gel Ni/Al\_2O\_3 catalysts reduced under H\_2 at 600  $^\circ C$  for 2 h

Catalyst	Percentage D <sup>a</sup>	MSA (m <sup>2</sup> /g) <sup>b</sup>
20% Ni/Al <sub>2</sub> O <sub>3</sub>	4.9	6.6
20% Ni-2% La/Al <sub>2</sub> O <sub>3</sub>	3.7	4.9
20% Ni-5% La/Al <sub>2</sub> O <sub>3</sub>	3.3	4.5
20% Ni-2% Ce/Al <sub>2</sub> O <sub>3</sub>	6.4	8.5
20% Ni-5% Ce/Al <sub>2</sub> O <sub>3</sub>	2.3	3.1
20% Ni-2% Yb/Al <sub>2</sub> O <sub>3</sub>	5.0	6.6
20% Ni-5% Yb/Al <sub>2</sub> O <sub>3</sub>	2.8	3.8

<sup>a</sup> Percentage nickel dispersion.

<sup>b</sup> Nickel surface area, m<sup>2</sup>/g.

nickel dispersion on the high surface area of sol–gel alumina could be due to the formation of NiAl<sub>2</sub>O<sub>4</sub>, which is rather difficult to reduce [29,30]. The amount of H<sub>2</sub> chemisorbed on pure sol–gel alumina is negligibly small, thus no correction on H<sub>2</sub> uptake values was made. The nickel dispersion and nickel surface area increase in the following order:

20% Ni-2% La/Al<sub>2</sub>O<sub>3</sub> < 20% Ni/Al<sub>2</sub>O<sub>3</sub>

 $\approx 20\%$ Ni - 2%Yb/Al<sub>2</sub>O<sub>3</sub> < 20%Ni-2%Ce/Al<sub>2</sub>O<sub>3</sub>

Additionally, the nickel dispersion and nickel surface area are seen to decrease at higher lanthanide content; a decrease is more pronounced with Ni–Ce/Al<sub>2</sub>O<sub>3</sub> and Ni–Yb/Al<sub>2</sub>O<sub>3</sub> catalysts. This implies that higher amounts of lanthanides could cover or block nickel sites for hydrogen adsorption.

The effect of calcination and reduction temperatures on the nickel dispersion and nickel surface area of Ni/Al<sub>2</sub>O<sub>3</sub> and Ni–Ce/Al<sub>2</sub>O<sub>3</sub> catalysts is further examined. As reported in Table 5, there are three major trends exhibited by the H<sub>2</sub> chemisorption data: (i) for the catalysts calcined at 450 °C, the nickel dispersion and nickel surface area increase with increasing reduction temperature and reach a maximum at 600 °C. Further increase in reduction temperature to 700 °C leads to a decrease in both parameters. It is conceivable that growth of nickel crystallites becomes more prominent with higher reduction temperatures; (ii) the nickel dispersion and nickel surface area increase with increasing reduction temperature for the catalysts calcined at 600 °C. In addition, the

Table 6

Propane steam reforming reaction data obtained with sol-gel Ni/Al2O3 catalysts-effect of synthesis parameters

#### Table 5

Effect of calcination ( $T_{cal}$ ) and reduction ( $T_{red}$ ) temperatures on nickel dispersion and surface area of sol–gel 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts

Catalyst	$T_{cal}$ (°C)	$T_{\rm red}$ (°C)	Percentage D <sup>a</sup>	MSA (m <sup>2</sup> /g) <sup>b</sup>
20% Ni/Al <sub>2</sub> O <sub>3</sub>	450	500	3.7	5.0
		600	4.9	6.6
		700	4.8	6.4
	600	500	3.3	4.4
		600	5.2	7.0
		700	5.4	7.2
20% Ni-2% Ce/Al <sub>2</sub> O <sub>3</sub>	450	500	5.2	6.9
		600	6.4	8.5
		700	6.2	8.3
	600	500	3.8	5.0
		600	6.2	8.2
		700	6.7	8.9

<sup>a</sup> Percentage nickel dispersion.

<sup>b</sup> Nickel surface area, m<sup>2</sup>/g.

catalysts exhibit higher nickel dispersion and larger nickel surface area at the reduction temperature of 700  $^{\circ}$ C compared to those calcined at 450  $^{\circ}$ C; and (iii) regardless of calcination and reduction temperatures, Ni–Ce/Al<sub>2</sub>O<sub>3</sub> catalysts possess higher nickel dispersion and larger nickel surface area than Ni/Al<sub>2</sub>O<sub>3</sub> catalysts.

# *3.4. Catalytic activity*

#### 3.4.1. Effect of synthesis parameters

The effect of catalyst synthesis parameters on the catalytic activity of sol–gel Ni/Al<sub>2</sub>O<sub>3</sub> catalysts at 500 °C and  $H_2O/C = 1.3$  is shown in Table 6. The parameters examined are Ni content, pH, and H<sub>2</sub>O/ATB ratio.

As reported in Table 6,  $C_3H_8$  conversion and  $H_2$  yield are seen to increase with increasing Ni content and reach a maximum at 20 wt.%, with  $C_3H_8$  conversion and  $H_2$  yield at 53 and 37%, respectively. Further increase in Ni content to 25 wt.% leads to a decline in catalytic activity. Moreover, the variations of pH and  $H_2O/ATB$  ratio also have a pronounced effect on catalytic activity of 20% Ni/Al<sub>2</sub>O<sub>3</sub>

Synthesis parameters		C <sub>3</sub> H <sub>8</sub> conversion (%)	H <sub>2</sub> yield (%)	Selectivity (%)			
Ni content (wt.%)	pH	H <sub>2</sub> O/ATB ratio			CO <sub>2</sub>	CH <sub>4</sub>	СО
10	4.8	3.6	16	21	85	0	15
15	4.8	3.6	27	33	73	19	8
20	4.8	3.6	53	37	54	36	10
25	4.8	3.6	43	29	52	31	17
20	4.8	3.6	53	37	54	36	10
20	7.0	3.6	31	28	61	20	19
20	8.8	3.6	27	26	68	20	12
20	4.8	3.6	53	37	54	36	10
20	4.8	4.0	43	30	63	30	7
20	4.8	5.0	23	23	77	15	8

Reaction conditions: 500 °C,  $C_3H_8/H_2O/N_2 = 1/4/95$ , feed flow rate = 300 cm<sup>3</sup>/min, equal surface area reactions (9 m<sup>2</sup>).

catalysts. The selectivities to C-containing products are also shown in Table 6. The C-containing products from propane steam reforming are CO, CO<sub>2</sub>, and CH<sub>4</sub> with CO<sub>2</sub> being the main one. CO<sub>2</sub> selectivity is seen to increase with a decrease in CH<sub>4</sub> selectivity at lower  $C_3H_8$  conversions. No CH<sub>4</sub> formation is observed at 10 wt.%.

#### 3.4.2. Effect of lanthanide promotion

Several sol–gel 20% Ni/Al<sub>2</sub>O<sub>3</sub> catalysts promoted with lanthanide elements (La, Ce, Yb) were subsequently prepared at pH=4.8 and H<sub>2</sub>O/ATB=3.6. The influence of lanthanide promotion (2 wt.%) on catalytic performance at different reaction temperatures is shown in Fig. 4. C<sub>3</sub>H<sub>8</sub> conversion (Fig. 4a) and H<sub>2</sub> yield (Fig. 4b) are seen to increase with increasing reaction temperature on all catalysts. Hydrogen yield that would be obtained at equilibrium is also included for comparison. 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> and 20% Ni–2% Yb/Al<sub>2</sub>O<sub>3</sub> catalysts show an improvement in C<sub>3</sub>H<sub>8</sub> conversion and H<sub>2</sub> yield compared to 20% Ni/Al<sub>2</sub>O<sub>3</sub> catalyst. Although 20% Ni–2% La/Al<sub>2</sub>O<sub>3</sub> catalyst exhibits similar C<sub>3</sub>H<sub>8</sub> conversion to 20% Ni/Al<sub>2</sub>O<sub>3</sub> catalyst, it still shows an increased H<sub>2</sub> yield above 450 °C. At 500 °C, the high-



Fig. 4. Effect of reaction temperature on catalytic performance of lanthanide-promoted sol-gel 20% Ni/Al<sub>2</sub>O<sub>3</sub> catalysts in propane steam reforming (a)  $C_3H_8$  conversion (b)  $H_2$  yield [reaction conditions: 400–500 °C,  $C_3H_8/H_2O/N_2 = 1/4/95$ , feed flow rate = 300 cm<sup>3</sup>/min, equal surface area reactions (9 m<sup>2</sup>)].

Table 7 Reaction comparison for propane steam reforming (dilution experiments) at 500 °C

Catalyst	C <sub>3</sub> H <sub>8</sub>	H <sub>2</sub> yield	Selectivity (%)		
	conversion (%)	(%)	$\overline{CO_2}$	$CH_4$	CO
20% Ni/Al <sub>2</sub> O <sub>3</sub>	53	37	54	36	10
20% Ni-2%La/Al <sub>2</sub> O <sub>3</sub>	51	40	59	28	13
20% Ni-5%La/Al <sub>2</sub> O <sub>3</sub>	29	29	55	29	16
20% Ni-2%Ce/Al <sub>2</sub> O <sub>3</sub>	72	46	50	38	12
20% Ni-5%Ce/Al <sub>2</sub> O <sub>3</sub>	53	38	56	33	11
20% Ni-2% Yb/Al <sub>2</sub> O <sub>3</sub>	84	50	46	38	16
20% Ni-5% Yb/Al <sub>2</sub> O <sub>3</sub>	65	44	50	35	15

Reaction conditions:  $500 \,^{\circ}$ C,  $C_3H_8/H_2O/N_2 = 1/4/95$ , feed flow rate = 300 cm<sup>3</sup>/min, equal surface area reactions (9 m<sup>2</sup>).

est  $C_3H_8$  conversion (84%) and  $H_2$  yield (50%) are achieved with 20% Ni–2% Yb/Al<sub>2</sub>O<sub>3</sub> catalyst. The effect of lanthanide promotion is more evident at higher reaction temperatures.

When the performances in propane steam reforming at different lanthanide contents are compared at 500 °C (Table 7), reaction data show that  $C_3H_8$  conversion and  $H_2$  yield decrease with increasing lanthanide content from 2 to 5 wt.%.  $H_2$  chemisorption data have also shown a decreasing trend of nickel surface area at higher lanthanide content. This indicates that the catalytic activity of lanthanide-promoted sol–gel Ni/Al<sub>2</sub>O<sub>3</sub> catalysts is strongly related to nickel surface area. Thus, loss of activity with higher lanthanide content is due to the blockage of active sites by excess amounts of lanthanides introduced in the catalysts. It is noted that the distribution of C-containing products is not much affected by an increase in lanthanide content.

To further investigate catalytic performance at higher reaction temperature, steady-state reaction experiments were conducted at 550 °C. However, the feed flow rate was raised to 400 cm<sup>3</sup> (STP)/min to avoid complete C<sub>3</sub>H<sub>8</sub> conversion. Interestingly, the highest C<sub>3</sub>H<sub>8</sub> conversion (80%) and H<sub>2</sub> yield (52%) are obtained with 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst at 550 °C (Table 8). Furthermore, 20% Ni–2% La/Al<sub>2</sub>O<sub>3</sub> catalyst also shows a significant improvement in steam reforming activity compared to 20% Ni/Al<sub>2</sub>O<sub>3</sub> catalyst under these reaction conditions. Moreover, an increase in CO selectivity is observed at higher reaction temperature. This suggests an increased contribution from the reverse water-gas shift reaction (CO<sub>2</sub> + H<sub>2</sub>  $\rightarrow$  CO + H<sub>2</sub>O) to the overall reaction network. Another possible explanation is that at higher

Table 8

Reaction comparison for propane steam reforming (dilution experiments) at 550  $^{\circ}\mathrm{C}$ 

Catalyst	C <sub>3</sub> H <sub>8</sub>	H <sub>2</sub> yield	Selectivity (%)		
	conversion (%)	(%)	$\overline{CO_2}$	$CH_4$	СО
20% Ni/Al <sub>2</sub> O <sub>3</sub>	48	36	48	21	31
20% Ni-2%La/Al <sub>2</sub> O <sub>3</sub>	66	52	38	25	37
20% Ni-2%Ce/Al <sub>2</sub> O <sub>3</sub>	80	52	31	32	37
20% Ni-2% Yb/Al2O3	70	50	33	30	37

Reaction conditions:  $550 \,^{\circ}$ C,  $C_3H_8/H_2O/N_2 = 1/4/95$ , feed flow rate = 400 cm<sup>3</sup>/min, equal surface area reactions (9 m<sup>2</sup>).

conversion, water becomes the limiting reactant, and leading to an increased formation of CO as opposed to  $CO_2$  from the steam reforming reaction. Increased coking on the surface at higher temperatures could also lead to higher CO formation through the gasification of surface carbon.

"Neat" experiments were performed with 20% Ni/Al<sub>2</sub>O<sub>3</sub>, 20% Ni-2% Ce/Al<sub>2</sub>O<sub>3</sub>, and 20% Ni-2% Yb/Al<sub>2</sub>O<sub>3</sub> catalysts in propane steam reforming without N2 dilution at the following conditions: T = 500-550 °C,  $H_2O/C = 4$ , total feed rate =  $270 \text{ cm}^3$  (STP)/min, equal surface area reaction (18 m<sup>2</sup>). Demineralized distilled water was delivered by an Eldex metering pump (model: A-10-S) connected with a 40 psi back pressure regulator and subsequently vaporized in a preheater which was operated above 150 °C. A column packed with ceramic beads was installed after the preheater to help C3H8 and steam mix effectively. The steady-state reaction experiments were performed using 1/2 in. o.d. stainless steel flow reactor to avoid high pressure drop due to higher amounts of catalysts loaded in the reactor. Consistent with reaction data obtained from dilution experiments, lanthanidepromoted catalysts give higher C<sub>3</sub>H<sub>8</sub> conversion and H<sub>2</sub> yield compared to the unpromoted catalyst (Table 9).

#### 3.4.3. Effect of calcination and reduction temperatures

When the effect of reduction temperature was examined by keeping the calcination temperature constant at  $450 \,^{\circ}$ C, a maximum is observed at a reduction temperature of  $600 \,^{\circ}$ C (Fig. 5). Both 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts give the highest H<sub>2</sub> yield when reduced at  $600 \,^{\circ}$ C. However, 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst gives superior performance at every reduction temperature. An improvement in H<sub>2</sub> yield with cerium promotion is much more evident at higher reduction temperatures. Furthermore, the catalytic activity of both catalysts calcined at  $450 \,^{\circ}$ C is seen to go

Table 9
Reaction comparison for propane steam reforming (neat experiments)

Catalyst	$T(^{\circ}C)$	C <sub>3</sub> H <sub>8</sub>	$H_2$ yield	Selectivity (%)		
		(%)	(70)	CO <sub>2</sub>	CH <sub>4</sub>	СО
20% Ni/Al <sub>2</sub> O <sub>3</sub>	500	35	14	68	25	7
	550	43	18	69	20	11
20% Ni-2%Ce/Al <sub>2</sub> O <sub>3</sub>	500	43	15	65	28	7
	550	95	31	58	28	14
200/ NF 20/ MI / 1 0	500	59	19	60	32	8
20% N1– $2%$ Y D/Al <sub>2</sub> O <sub>3</sub>	550	83	27	58	30	12

Reaction conditions: 500-550 °C,  $H_2O/C = 4$ , total feed rate = 270 cm<sup>3</sup>/min, equal surface area reaction (18 m<sup>2</sup>).

through a maximum at the reduction temperature of 600 °C and decreases at higher reduction temperature. By comparing the performance of 20% Ni-2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts calcined at 450 and 600 °C, we see that higher calcination temperature causes a decline in catalytic activity (Fig. 5b). The optimum reduction temperature is 600 °C regardless of calcination temperature. This observation is in good agreement with TPR results. When Ni-Ce/Al<sub>2</sub>O<sub>3</sub> catalysts are calcined at higher temperature (600 °C), NiO interacts with Al<sub>2</sub>O<sub>3</sub> to form a very stable NiAl<sub>2</sub>O<sub>4</sub> spinel which is more difficult to reduce [31–35]. However, we cannot explain the lower activity of the catalyst calcined at 600 °C when it is reduced at 700 °C. As previously discussed, the catalysts calcined at higher temperature exhibit higher nickel dispersion and nickel surface area when reduced at 700 °C (Table 5). Our in situ X-ray diffraction studies performed to observe the phase changes during reduction have shown incomplete reduction at lower temperatures while Ni sintering was observed at higher temperatures [36].



Fig. 5. Effect of calcination and reduction temperatures on catalytic performance in propane steam reforming (a) comparison between 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts calcined at 450 °C; (b) effect of calcination temperature on 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts [reaction conditions: 550 °C, H<sub>2</sub>O/C = 2, GHSV = 248,000 h<sup>-1</sup>].



Fig. 6. Effect of GHSV on  $H_2$  yield in propane steam reforming over 20%  $Ni/Al_2O_3$  and 20% Ni-2% Ce/Al\_2O\_3 catalysts: (a) 500  $^\circ\text{C}$  and (b) 550  $^\circ\text{C}$ .

#### 3.4.4. Effect of gas hourly space velocity (GHSV)

The catalytic performance of 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni-2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts in propane steam reforming was further investigated at various space velocities. The reaction conditions for these experiments were as follows: 500-550 °C, H<sub>2</sub>O/C = 2. The variation of GHSV was performed by adjusting both the amount of the catalyst (10-20 mg) and the feed flow rate  $(200-400 \text{ cm}^3 \text{ (STP)/min})$ . As expected, H<sub>2</sub> yield increases with decreasing GHSV from 496,000 to  $124,000 \text{ h}^{-1}$  over both catalysts (Fig. 6). At 500 °C, the beneficial effect of cerium promotion becomes much more pronounced at lower GHSVs. At 550°C, an improvement in H<sub>2</sub> yield with the addition of cerium is evident for the whole range of GHSVs examined. C3H8 conversion rates at steady state were further normalized to surface nickel atoms, measured by H<sub>2</sub> chemisorption at 35 °C, in the form of turnover frequencies (TOFs). Table 10 compares average TOFs obtained with 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni-2%

Table 10

Effect of reaction temperature on turnover fi	requency
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Catalyst	TOF (s <sup>-1</sup> )		
	500 °C	550°C	
20% Ni/Al <sub>2</sub> O <sub>3</sub>	0.35	0.65	
20% Ni-2%Ce/Al <sub>2</sub> O <sub>3</sub>	0.50	1.20	

Table 11 Comparison of CO-methanation activity of 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts

Catalyst	CH <sub>4</sub> yield (%)		CO <sub>2</sub> yield (%)	
	500 °C	550°C	500 °C	550 °C
20% Ni/Al <sub>2</sub> O <sub>3</sub>	59	46	5	5
20% Ni-2%Ce/Al <sub>2</sub> O <sub>3</sub>	71	61	5	5

Reaction conditions:  $F_{CO} = 10 \text{ cm}^3$  (STP)/min, CO/H<sub>2</sub>/N<sub>2</sub> = 1/6/13, GHSV = 372,000 h^{-1}.

Ce/Al<sub>2</sub>O<sub>3</sub> catalysts at 500 and 550 °C. TOF is seen to increase with increasing reaction temperature. The increase is more pronounced with 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst. Furthermore, the higher activity of promoted catalysts is clearly seen when TOF values are compared for the 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> and 20% Ni/Al<sub>2</sub>O<sub>3</sub> catalysts.

The variation of product selectivities with  $C_3H_8$  conversion over 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts is shown in Fig. 7. In this study, CO<sub>2</sub> selectivity is defined as the ratio of moles of CO<sub>2</sub> produced to the total moles of C-containing products (i.e., CO<sub>2</sub>, CO, and CH<sub>4</sub>) whereas H<sub>2</sub> selectivity is defined as 2 × moles of H<sub>2</sub> produced/total moles of hydrogen in the H-containing products, which are H<sub>2</sub> and CH<sub>4</sub>. Interestingly, CH<sub>4</sub> selectivity is seen to increase at the expense of both H<sub>2</sub> and CO<sub>2</sub> selectivities at lower GHSVs, i.e., higher conversions. This suggests that CO<sub>2</sub> methanation (CO<sub>2</sub> + 4H<sub>2</sub>  $\rightarrow$  CH<sub>4</sub> + 2H<sub>2</sub>O) becomes more appreciable when residence time is increased, leading to an increased CH<sub>4</sub> selectivity. CO selectivity, on the other hand, is not much affected by the variation of C<sub>3</sub>H<sub>8</sub> conversion over either catalyst.

The CO- and CO<sub>2</sub>-methanation reactions over 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts were further investigated at 500–550 °C. The H<sub>2</sub>/CO and H<sub>2</sub>/CO<sub>2</sub> ratios for these experiments were kept constant at 6. CH<sub>4</sub> yield is defined as moles of carbon in CH<sub>4</sub> produced/total moles of carbon in the feed. As shown in Tables 11 and 12, CH<sub>4</sub> yield is seen to decrease with increasing reaction temperature over both catalysts. Ce-promoted catalyst shows higher CH<sub>4</sub> yields from both CO- and CO<sub>2</sub>-methanation reactions compared to unpromoted catalyst. It is worth noting that a lower level of CH<sub>4</sub> produced from the CO<sub>2</sub>-methanation reaction at 550 °C implies an increased contribution from the reverse water-gas shift reaction at higher temperature. Ross and co-workers [37,38] studied the CO-methanation reaction

Table 12
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Comparison of CO2-methanation activity of 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts

Catalyst	CH <sub>4</sub> yield (%)		CO yield (%)	
	500 °C	550°C	500 °C	550 °C
20% Ni/Al <sub>2</sub> O <sub>3</sub>	14	13	28	36
20% Ni-2%Ce/Al <sub>2</sub> O <sub>3</sub>	30	22	24	34

Reaction conditions:  $F_{CO_2} = 15 \text{ cm}^3$  (STP)/min,  $CO_2/H_2/N_2 = 1/6/20$ , GHSV = 496,000 h<sup>-1</sup>.



Fig. 7. Variation of product selectivities with C3H8 conversion.

on coprecipitated Ni/Al<sub>2</sub>O<sub>3</sub> catalysts promoted with La<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub>. An enhancement in methanation activity was observed with an increase in apparent activation energy upon lanthanide promotion. The role of lanthanum and cerium in the methanation reaction was reported to be associated with higher amounts of CO and H<sub>2</sub> adsorbed on nickel surface due to an interaction between lanthanides and nickel in the catalysts. Our H<sub>2</sub> chemisorption studies have shown that 20% Ni-2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst shows an increased H<sub>2</sub> uptake compared to 20% Ni/Al<sub>2</sub>O<sub>3</sub> catalyst, thus resulting in higher nickel dispersion and larger nickel surface area (Table 4). Furthermore, the CO uptakes measured by CO chemisorption at 35 °C are 3.39 and 10.16 cm<sup>3</sup>/ $g_{cat}$  over 20% Ni/Al<sub>2</sub>O<sub>3</sub> and 20% Ni-2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts reduced at 600 °C, respectively. Consequently, an improvement in methanation activity when cerium is added into sol-gel Ni/Al2O3 catalysts could be due to an increased CO and H<sub>2</sub> adsorption on nickel crystallites. A higher amount of CO2 adsorbed on nickel upon cerium promotion could also be another possibility.

### 3.5. DRIFTS studies

#### 3.5.1. $C_3H_8$ -TPD/TPReaction

TPD/TPReaction experiments with DRIFTS were performed over reduced 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst, where strongly adsorbed propane was allowed to react with water. Adsorption of propane was carried out at room temperature for 1 h. The system was subsequently purged and heated under He and spectra were collected in steps under He flow up to 450 °C. The introduction of H<sub>2</sub>O was performed at 450 °C for different times on stream (i.e., 5, 10, and 15 min) followed by He flushing before spectra were taken.

Fig. 8 shows DRIFT spectra taken at 25, 100, 200, 250, 300, and 450 °C under He after  $C_3H_8$  adsorption over reduced 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst. After propane adsorption and He flushing, bands remained at 2940, 2932 (shoulder), 2824, 1630, 1476, 1435 (shoulder), 1373, 1189, and 1103 cm<sup>-1</sup> at room temperature. The band at 1630 cm<sup>-1</sup> could be attributed to an olefinic C=C vibration [39,40]



<sup>•</sup>H,O, 15 min

Fig. 8. DRIFT spectra taken over reduced 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts after  $C_3H_8$  adsorption; \*H<sub>2</sub>O was introduced for 5, 10, and 15 min and the system was flushed under He for 5 min.

and has been observed in a separate propylene adsorption/desorption DRIFTS experiment performed in our laboratory (Fig. 9). However, bands typical of olefinic sp<sup>2</sup> C–H stretching present above  $3000 \text{ cm}^{-1}$  were not observed after propane adsorption which leads us to assume that the band at  $1630 \text{ cm}^{-1}$  could be assigned as the O-H bending frequency of adsorbed water as observed by Gates and co-workers [41]. The remaining bands are characteristic of adsorbed propylidyne [39,42] and are similar to resultant spectra of propane adsorbed on a reduced Ir/Al<sub>2</sub>O<sub>3</sub> catalyst [41]. In addition, a



Fig. 9. DRIFT spectra taken over reduced 20% Ni–2% Ce/Al $_2O_3$  catalysts after  $C_3H_6$  adsorption at room temperature.

negative peak at  $3750 \,\mathrm{cm}^{-1}$ , which is characteristics of surface hydroxyl groups on the alumina support, was observed [43,44]. This indicates that the surface hydroxyl groups either interacted with propane or were consumed upon the adsorption of propane. Although the intensities of the bands at 2940 and 2824  $\rm cm^{-1}$  decreased at higher temperatures, they were thermally stable up to 450 °C. The features at 2940 and 2932 cm<sup>-1</sup> are assigned to asymmetric CH<sub>3</sub> stretching  $[\nu_{as}(CH_3)]$  and asymmetric CH<sub>2</sub> stretching  $[\nu_{as}(CH_2)]$ , respectively [39,42,45-47]. The feature at  $2824 \text{ cm}^{-1}$  could be attributed to either symmetric CH<sub>2</sub> stretching  $[v_s(CH_2)]$  or symmetric CH<sub>3</sub> stretching  $[v_s(CH_3)]$  [42,48]. The features at 1476, 1437, 1373, 1189, and 1103 cm<sup>-1</sup> decreased in intensity with temperature and subsequently almost disappeared at 300 °C. These features could be associated with adsorbed ethylidyne/propylidyne species that were depleted upon the reaction with H<sub>2</sub>O. At 450 °C and before the introduction of water, new bands at 1600 and 1374 cm<sup>-1</sup> were present accompanied by two small C-H stretching bands at 2954 and  $2904 \text{ cm}^{-1}$ . Although it is conceivable that new CH<sub>3</sub> groups could be forming due to desorption/re-adsorption processes, a more likely explanation is that the features at 2954, 2904, 1600, and  $1374 \text{ cm}^{-1}$  are due to formate species [49,50]. With the introduction of water at 450 °C, the bands associated with the formate species grew much stronger and were seen in higher intensity with time on stream. In the course of propane steam reforming, formate species are probably produced by the reaction of CO with the water introduced. In the absence of water, surface hydroxyl groups can serve as a source of oxygen to form formate species. Our formate band assignments are consistent with those which arise from adsorption of CO on 1% Au/ceria and 1% Pt/ceria catalysts [51]. Two additional features at 1455 and  $1255 \text{ cm}^{-1}$ , which could be attributed to carbonate species, were also observed after H<sub>2</sub>O exposure at  $450 \degree C$  [49,50].

In order to help in the band assignments for the  $C_3H_8$ -TPD/TPReaction experiment, DRIFT spectra were taken after propylene and CO<sub>2</sub> adsorption in separate experiments. Fig. 9 shows DRIFT spectra taken at 25, 250, and 450 °C under He flow over reduced 20% Ni-2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst during the C<sub>3</sub>H<sub>6</sub>-TPD experiment. The strong presence of the band at 1630 cm<sup>-1</sup> on the catalyst surface following propylene adsorption signals the C=C stretching vibration. Presence of olefinic C-H vibrations that would be expected above  $3000 \,\mathrm{cm}^{-1}$  cannot be discerned from this spectrum due to a very broad feature in that region. It is possible that adsorbed propylene could be dehydrogenated on the surface, giving rise to water (surface hydroxyl groups), which would show an IR band around 1630 cm<sup>-1</sup> as well as a broad feature above  $3000 \text{ cm}^{-1}$ . The feature at  $1373 \text{ cm}^{-1}$ , which was quite prominent following propane adsorption, could not be observed after propylene adsorption. This observation supports the assignment of the band at  $1373 \text{ cm}^{-1}$  to symmetric CH<sub>3</sub> bending  $[\delta_s(CH_3)]$  of propylidyne. This assignment is in agreement with what is reported by Shahid and Sheppard [42]. In addition, the feature at  $2824 \text{ cm}^{-1}$  was absent,



Fig. 10. DRIFT spectra taken over reduced 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts after CO<sub>2</sub> adsorption at room temperature.

and the 2940 cm<sup>-1</sup> band was much weaker and disappeared very quickly at higher temperatures. The band at 1476 cm<sup>-1</sup>, which was quite strong following propane adsorption was barely noticeable ( $\sim$ 1456 cm<sup>-1</sup>) after propylene adsorption. This observation makes us believe that this feature could be due to a methyl group, which may have a different orientation in species resulting from propylene adsorption. This explanation would also be consistent with our earlier assertion that propylidyne species are the predominant hydrocarbon derivatives on the surface following propane adsorption, but this is not necessarily the case following propylene adsorption.

From DRIFT spectra of CO2-TPD over the reduced 20% Ni-2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst, bands at 3619, 2355, 2325, 1643, 1543 (shoulder), 1438, 1387 (shoulder), 1229, and  $1084 \text{ cm}^{-1}$  are seen at room temperature (Fig. 10). The bands at 3619, 1643, 1438, and 1229 cm<sup>-1</sup> are assigned to bicarbonate species and decrease in intensity significantly at 250 °C [49,50,52]. Conversely, carbonate species are characterized by the shoulder bands at 1543, and 1387  $\text{cm}^{-1}$  as well as the  $1084 \,\mathrm{cm}^{-1}$  band [49,50,52]. In addition, the only other feature observed is a doublet at 2355 and  $2325 \text{ cm}^{-1}$ , which corresponds to adsorbed CO<sub>2</sub> [53,54]. The disappearance of carbonate and bicarbonate species at higher temperatures leads us to believe that formate and carbonate species observed from the C3H8-TPD/TPReaction experiment are the result of the surface transformation of propylidyne species rather than from the re-adsorption of CO<sub>2</sub>.

# 3.5.2. $C_3H_8 + H_2O$ -TPReaction

 $C_3H_8 + H_2O$ -TPReaction with DRIFTS was also performed over reduced 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalyst.  $C_3H_8$ was adsorbed at room temperature for 1 h. The system was then purged under He for 30 min and H<sub>2</sub>O was subsequently introduced for 5 min at room temperature followed by He flushing for 5 min. The system was heated and DRIFT spec-



Fig. 11. DRIFT spectra taken over reduced 20% Ni–2% Ce/Al<sub>2</sub>O<sub>3</sub> catalysts after consecutive adsorption of  $C_3H_8$  and  $H_2O$ .

tra were collected in steps under He flow up to  $450 \,^{\circ}$ C. It is noted that H<sub>2</sub>O was re-introduced at each temperature for 5 min followed by He flushing before taking spectra.

After C<sub>3</sub>H<sub>8</sub> and H<sub>2</sub>O introduction at room temperature, bands remained at 3750-3500 (very broad), 2940, 2824, 2055, 1630, 1435 (weak), 1373 (weak), and 1255 (weak) cm<sup>-1</sup> (Fig. 11). The broad band around  $3750-3500\,\mathrm{cm}^{-1}$  is characteristic of the OH stretching region while the feature at  $2055 \text{ cm}^{-1}$  is assigned to linearly adsorbed CO on the catalyst surface and disappeared above 200 °C [55-57]. Compared to the DRIFT spectrum after C<sub>3</sub>H<sub>8</sub> adsorption at room temperature, the intensity of the band located at 1630 cm<sup>-1</sup> increased significantly when H<sub>2</sub>O was introduced at room temperature. This band decreased in intensity at higher temperatures and eventually shifted to  $1600 \text{ cm}^{-1}$  at  $450 \,^{\circ}\text{C}$ . The band at  $1600 \text{ cm}^{-1}$ is attributed to a formate species as previously observed from the C<sub>3</sub>H<sub>8</sub>-TPD/TPReaction experiment. The features at 2940 and  $2824 \text{ cm}^{-1}$  were seen in much lower intensity and disappeared above 250 °C whereas the bands at 2954 and 1455 cm<sup>-1</sup> started to appear at 200 °C and grew stronger at higher temperatures. Furthermore, two additional bands at 2904 and 1374 were seen at 450 °C. It is evident that most surface species such as formate and carbonate ions are formed upon the reaction of adsorbed C3H8 and H2O above 250 °C. In a separate experiment with C<sub>3</sub>H<sub>8</sub> + H<sub>2</sub>O adsorption in a reverse order (not shown), a large band at 1645 cm<sup>-1</sup> was also observed after water adsorption at room temperature. This observation provides additional support for our earlier assertion that the  $1630 \text{ cm}^{-1}$  feature seen in the C<sub>3</sub>H<sub>8</sub>-TPD/TPReaction and C<sub>3</sub>H<sub>8</sub> + H<sub>2</sub>O-TPReaction experiments is due to adsorbed water. Interestingly, no additional features



Fig. 12. Possible mechanistic steps during propane steam reforming over reduced Ni–Ce/Al<sub>2</sub>O<sub>3</sub> catalyst as observed using in situ DRIFTS.

were seen following  $C_3H_8$  adsorption, suggesting water could be primarily adsorbed on metallic nickel sites and therefore inhibits the adsorption of propane.

Based on the observed surface specie transformations from in situ DRIFTS studies, the following major reaction pathways for adsorbed propane in the presence of steam over reduced sol-gel Ni-Ce/Al<sub>2</sub>O<sub>3</sub> catalysts are proposed as illustrated in Fig. 12. The first step is believed to be adsorption of propane on metallic nickel sites to form propylidyne. To a lesser degree, adsorbed propane can further decompose into hydrocarbon fragments (i.e.,  $CH_x$ ) and even carbon oxides in the presence of adsorbed water. Carbon deposition, especially at higher temperatures, also is a possibility as seen through our coking studies [36]. During this step, it is likely that the formation of carbon monoxide could be occurring on nickel sites. Adsorbed water from the catalyst can combine with adsorbed hydrocarbon fragments or adsorbed carbon monoxide to form formate species. It is also possible that adsorbed hydrocarbon fragments could react with other sources of oxygen (hydroxyls, ceria lattice) to form formates in the absence of water, as observed at 450 °C (Fig. 8). Additionally, it is possible that water could dissociatively adsorb to produce gaseous hydrogen and surface oxygen species. These surface oxygen species have been found to react with methane to form CO and hydrogen in methane steam reforming over various oxide supports, including ceria [58-60]. Unfortunately, we cannot obtain information pointing to the dissociative adsorption of water to form hydrogen from the DRIFTS experiments. However, the contribution from hydroxyls created from adsorbed water is expected to be much higher than that from surface oxygen. The thermal decomposition of adsorbed formates can result in the formation of carbon dioxide and hydrogen, or the formation of carbon monoxide and

hydroxyl groups [50]. Moreover, the fraction of the formate remaining adsorbed could react with hydroxyl groups arising from adsorbed water to form carbonates and hydrogen at higher temperatures. While the DRIFTS experiments do not specifically indicate the participation of other surface intermediates, it could be possible that adsorbed species such as oxygen atoms, hydrogen atoms, and hydroxyl groups could also be spilling over to the nickel surface from the alumina support or ceria, thus enhancing the overall adsorption and participation of water.

#### 4. Conclusions

Various sol-gel Ni/Al2O3 catalysts promoted with lanthanide elements (La, Ce, and Yb) were studied in the steam reforming of propane. The promotion effect is most pronounced on the Ni-Ce/Al<sub>2</sub>O<sub>3</sub> catalysts. An improvement in catalytic activity with respect to C<sub>3</sub>H<sub>8</sub> conversion and H<sub>2</sub> yield appears to be due to easier reduction of nickel species to a metallic state and larger nickel surface area. Additionally, cerium promotion enhances the CO- and CO<sub>2</sub>-methanation activity, leading to an increased CH<sub>4</sub> yield. DRIFT experiments suggest adsorbed propylidyne to be the predominant surface species following C3H8 adsorption at room temperature and to subsequently react with hydroxyl groups arising from adsorbed water to form formate and carbonate species at higher temperatures. The second paper of this series [36] examines the effect of lanthanide promotion in terms of the deactivation characteristics of these catalysts under steam reforming conditions.

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